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NUMERICAL STUDIES OF FLOW BETWEEN ROTATING COAXIAL DISKS

by

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ABSTRACT

A new algorithm, which is exceptionally fast for certain choices of numerical parameters, is described for the study of nonlinear, incompressible flow between two rotating disks. Typical examples for Reynolds number R in the range $10 \le R \le 2000$ are described and discussed. Comparisons are made with the limited available results generated by other methods.

1. INTRODUCTION

The study of fluid motion between rotating disks is of both practical and theoretical interest (see, e.g., references [1]-[7], [9]-[17], [18]-[25], and the references contained therein). It appears that the first mathematical paper on the subject was that of von Karmen [24], who dealt with the steady flow above an infinitely large rotating disk under the assumption that axial velocity was radius independent. This model was extended to steady flow between two coaxial rotating disks by Batchelor [2], and then to nonsteady models by Greenspan [9], Greenspan and Howard [10], and Pearson [15]. In studying the related mathematical and physical problems, various techniques have been applied, including asymptotic analysis ([2], [6], [20]-[22], [25]), linearization [10], [11], [16], numerical analysis [5], [12], [13], [15], [16], and experimentation [13], [21]. Unfortunately, the results of these analyses often are either unreasonable or contradictory. Thus, as the Reynolds number becomes infinite, Batchelor [2] and Stewartson [21] both find unique, steady, limiting flows, but which are qualitatively different, while Tam [22] claims that the problem admits an infinite number of flows. Pearson [15] and Lance and Rogers [12], using different numerical techniques, generate qualitatively different [lows for certain classes of nonsteady problems. Mellor, Chapple and Stokes [13] claim to have produced several classes of solutions for a given

problem by analytical-numerical means, but then can produce only one such class in laboratory experiments.

Our purpose in this paper is to study numerically only the steady motion of a viscous, incompressible fluid between two rotating, infinite coaxial disks. For simplicity, the first disk is positioned in (x,y,z) space in the plane z=0 with its center at (0,0,0) and is given an angular velocity Ω_1 , while the second disk is positioned in the plane z=1 with its center at (0,0,1) and is given an angular velocity Ω_2 . If the cylinderical coordinates of (x,y,z) are (r,θ,z) , and if the fluid at (x,y,z) has velocity components (u,v,w), then the substitutions

(1.1)
$$u = -\frac{1}{2} r H'(z), v = r G(z), w = H(z)$$

enable one ([9], [15]) to transform the dimensionless, steady state Navier-Stokes equations to

$$(1.2)$$
 $H'' = M$, $0 \le z \le 1$

(1.3)
$$G'' + R(GH' - G'H) = 0$$
 , $0 \le z \le 1$

(1.4)
$$M'' - R(HM' + 4GG') = 0$$
 , $0 \le z \le 1$,

where differentiation is with respect to z. For the coaxial flow under consideration, the boundary conditions for nonlinear system (1.2)-(1.4) are ([9], [15])

(1.5)
$$G(0) = \Omega_1$$
, $G(1) = \Omega_2$

$$(1.6)$$
 $H(0) = 0$, $H(1) = 0$

$$(1.7)$$
 $H'(0) = 0$, $H'(1) = 0$.

The numerical method to be used is an extension of one developed for cavity flow problems [8], and which was convergent for all Reynolds numbers studied ($0 \le R \le 10^6$). Since the present work is largely experimental in nature, and since errors in computation often seem to be more the rule than the exception, the FORTRAN program used is being made accessible in a report [18], so that every aspect of the calculations can be reproduced by the reader.

2. THE NUMERICAL METHOD

In this section we give a precise description of the algorithm to be used for the numerical solution of (1.2)-(1.7).

Divide $0 \le z \le 1$ into n equal parts, each of length $h = \Delta z = \frac{1}{n}$. Let the points of subdivision be $0 = z_0 < z_1 < z_2 < \cdots < z_n = 1$. Thus, $z_j = jh = \frac{j}{n}$, $j = 0, 1, 2, \ldots, n$. Let S_h be the set of boundary grid points z_0 and z_n , while I_h is the set of interior grid points z_1 , z_2, \ldots, z_{n-1} . If F is any function defined on $S_h + I_h$, then a convenient notation will be

$$F(z_i) = F_i.$$

We attempt to approximate H, G, and M by generating three sequences, $H^{(k)}$, $G^{(k)}$, and $M^{(k)}$, $k=0,1,2,\ldots$, on I_h+S_h , each of which is convergent. This is done as follows. For all values of k, let

(2.1)
$$H_0^{(k)} = H_n^{(k)} = 0$$
, $k = 0, 1, 2, ...$

(2.2)
$$G_0^{(k)} = \Omega_1, G_0^{(k)} = \Omega_2, k = 0,1,2,...$$

Set

(2.3)
$$H_i^{(0)} = 0$$
 , $i = 1, 2, ..., n-1$

(2.4)
$$G_i^{(0)} = (1-z)\Omega_1 + z\Omega_2$$
, $i = 1, 2, ..., n-1$

(2.5)
$$M_i^{(0)} = 0$$
 , $i = 0, 1, 2, ..., n$.

By induction, $H^{(k+1)}$, $G^{(k+1)}$ and $M^{(k+1)}$ are generated from $H^{(k)}$, $G^{(k)}$ and $M^{(k)}$ as is shown next.

At the points z_1 and z_{n-1} write down the two equations

$$(2.6) 4H_1 = H_2$$

$$(2.7) 4H_{n-1} = H_{n-2},$$

which are difference approximations (see [4])of (1.7). At each of the remaining points of $I_{\rm h}$, write down the difference analogue

(2.8)
$$H_{i-1} - 2H_i + H_{i+1} = h^2 M_i^{(k)}, i = 2,3,...,n-2$$

of (1.2). Insertion of (2.1) into (2.6)-(2.8) results in a diagonally dominant linear algebraic system. Solve this system by SOR (point successive over-relaxation) with over-relaxation factor r_H and convergence tolerance α_1 , and denote the solution by $H_i^{(k+1)}$, $i=1,2,\ldots,n-1$. Define $H_i^{(k+1)}$, $i=1,2,\ldots,n-1$, by the smoothing formula

(2.9)
$$H_{i}^{(k+1)} = \rho \overline{H}_{i}^{(k+1)} + (1 - \rho) H_{i}^{(k)}, \qquad \begin{cases} i = 1, 2, \dots, n-1 \\ k = 0, 1, 2, \dots \\ 0 \le \rho \le 1 \end{cases}$$

At each point of I_h , write down next the following forward-backward difference analogues of (1.3):

$$(2.10) \quad G_{i-1} + \left[-2 + RhH_{i}^{(k+1)}\right]G_{i} + \left[1 - RhH_{i}^{(k+1)}\right]G_{i+1}$$

$$= -\frac{1}{2}RhG_{i}^{(k)}\left[H_{i+1}^{(k+1)} - H_{i-1}^{(k+1)}\right]; \quad \text{if} \quad H_{i}^{(k+1)} < 0,$$

$$(2.11) \quad [1 + RhH_{i}^{(k+1)}]G_{i-1} + [-2 - RhH_{i}^{(k+1)}]G_{i} + G_{i+1}$$

$$= -\frac{1}{2}RhG_{i}^{(k)}[H_{i+1}^{(k+1)} - H_{i-1}^{(k+1)}]; \text{ if } H_{i}^{(k+1)} \ge 0.$$

Solve the resulting diagonally dominant linear algebraic system by SOR with over-relaxation factor ${\bf r}_G$ and convergence tolerance α_2 , call the solution $\bar{\bf G}^{(k+1)}$, and on ${\bf I}_h$ define ${\bf G}^{(k+1)}$ by

(2.12)
$$G_{i}^{(k+1)} = \mu \, \overline{G}_{i}^{(k+1)} + (1 - \mu) G_{i}^{(k)}, \begin{cases} i = 1, 2, \dots, n-1 \\ k = 0, 1, 2, \dots \\ 0 \le \mu \le 1. \end{cases}$$

Note that (2.10)-(2.11) avoid the possible eigenvalue problems inherent in viewing (1.3) as an equation in G by using the iterate $G^{(k+1)}$ to approximate G' and G' and using the iterate $G^{(k)}$ to approximate G.

To construct $M^{(k+1)}$ on $I_h + S_h$, first set (see [4])

$$(2.13) M_0^{(k+1)} = \delta_1 \left[2H_1^{(k+1)}/h^2 \right] + (1 - \delta_1) M_0^{(k)}, \begin{cases} k = 0,1,2,\dots \\ 0 \le \delta_1 \le 1 \end{cases}$$

(2.14)
$$M_n^{(k+1)} = \delta_1 \left[2H_{n-1}^{(k+1)}/h^2 \right] + (1 - \delta_1) M_n^{(k)}, \qquad \begin{cases} k = 0, 1, 2, \dots \\ 0 \le \delta_1 \le 1. \end{cases}$$

Using (2.13) and (2.14) as boundary values, write down at each point of I_h the following forward-backward difference analogues of (1.4):

$$(2.15) M_{i-1} + [-2 + RhH_i^{(k+1)}]M_i + [1 - RhH_i^{(k+1)}]M_{i+1}$$

$$= 2Rh G_i^{(k+1)} [G_{i+1}^{(k+1)} - G_{i-1}^{(k+1)}], if H_i^{(k+1)} < 0,$$

$$\begin{aligned} & (2.16) \quad \left[1 + \text{Rh}H_{i}^{(k+1)}\right] M_{i-1} + \left[-2 - \text{Rh}H_{i}^{(k+1)}\right] M_{i} + M_{i+1} \\ & = 2\text{Rh}\,G_{i}^{(k+1)} \quad \left[G_{i+1}^{(k+1)} - G_{i-1}^{(k+1)}\right], \quad \text{if} \quad H_{i}^{(k+1)} \geq 0. \end{aligned}$$

Solve the resulting diagonally dominant, linear algebraic system by SOR with successive over-relaxation factor $r_{\rm M}$ and convergence tolerance α_3 , call the solution $\bar{M}^{(k+1)}$, and define $M^{(k+1)}$ on $I_{\rm h}$ by

$$(2.17) \quad M_{i}^{(k+1)} = \delta_{2} \overline{M}_{i}^{(k+1)} + (1 - \delta_{2}) M_{i}^{(k)}, \quad \begin{cases} i = 1, 2, \dots, n-1 \\ k = 0, 1, 2, \dots \\ 0 \le \delta_{2} \le 1 \end{cases}$$

For given positive tolerances ϵ_1 , ϵ_2 , ϵ_3 , the iteration proceeds for $k=0,1,2,\ldots$, until for some value k=K, one has

(2.18)
$$\left| \; H^{(K+1)} - H^{(K)} \right| < \; \epsilon_{1} \; \text{, uniformly in } \; I_{h}$$

(2.19)
$$\left| \; G^{(K+1)} - G^{(K)} \; \right| \; < \; \epsilon_{_{\hbox{$\mbox{$Z$}}}} \; , \; \mbox{uniformly on } \; I_{_{\hbox{$\mbox{$h$}}}}$$

$$|\,M^{(K+1)}-M^{(K)}\,|\,<\,\epsilon_3^{}\,\,,\,\,{\rm uniformly\,\,on}\,\,\,I_h^{}+\,S_h^{}.$$

Finally one verifies whether or not $H^{(K+1)}$, $G^{(K+1)}$, $M^{(K+1)}$ are solutions of the difference equations being solved, and, if they are, then they are taken to be the respective approximations of H, G, M.

3. EXAMPLES

From the large number of examples run on the UNIVAC 1108, several which are typical, which are of physical interest, and which display readily the changes of flow patterns with increasing Reynolds number, will be presented in this section.

For h = $\frac{1}{50}$, Ω_1 = 1, and Ω_2 = 0, the results for H, H' and G, with H' determined by central differences, are shown graphically for Reynolds numbers 10, 100, 1000 in Figures 1, 2, 3, respectively. The other parameter choices were: (a) for R = 10, ρ = 0.9, μ = 0.9, μ = 0.8, μ = 0.8, μ = 0.1, μ = 1.8, μ = 1.0, μ = 1.1, μ = 1.8, μ = 1.0, μ = 1.5, μ = 1.8, μ = 1.8, μ = 1.1, μ = 1.5, μ = 1.5, μ = 1.5, μ = 1.8, μ = 1.8, μ = 1.1, μ = 1.5, μ = 1.5, μ = 1.5, μ = 1.8, μ = 1.8, μ = 1.9, μ = 1.5, μ = 1.9, μ = 1.8, μ = 1.9, μ

(3.1)
$$H^{(0)}(z) = \begin{cases} -0.6z, & 0 \le z \le \frac{1}{2} \\ (0.6)(z-1), & \frac{1}{2} \le z \le 1 \end{cases}$$

(3.2)
$$M^{(0)}(z) = \begin{cases} -12 + 36z, & 0 \le z \le \frac{1}{2} \\ -6 - 24(z - 1), & \frac{1}{2} \le z \le 1, \end{cases}$$

respectively, at the grid points, and convergence was attained in 19 outer iterations. Choices (3.1) and (3.2) were motivated by the results for R = 100 shown in Figure 2. The maximum running time of all cases discussed thus far was under thirty seconds and convergence resulted for a variety of other choices of parameters.

In $h=\frac{1}{50}$, $\Omega_1=1$, and $\Omega_2=-1$, the results for H, H' and G are shown graphically for Reynolds numbers 10, 100, 1000 in Figures 4, 5, 6, respectively. The other parameter choices were: (a) for R=10, $\rho=0.9$, $\mu=0.9$, $\delta_1=0.8$, $\delta_2=0.1$, $r_H=1.8$, $r_G=1.0$, $r_M=1.0$, $\alpha_1=\alpha_2=\alpha_3=\epsilon_1=\epsilon_2=\epsilon_3=0.005$, (b) for R=100, $\rho=0.9$, $\mu=0.2$, $\delta_1=0.8$, $\delta_2=0.1$, $r_H=1.8$, $r_G=1.0$, $r_M=1.5$, $\alpha_1=\alpha_2=\epsilon_1=\epsilon_2=0.001$, $\alpha_3=\epsilon_3=0.05$, (c) for R=1000, $\rho=0.1$, $\mu=0.1$, $\delta_1=0.05$, $\delta_2=0.9$, $r_H=1.8$, $r_G=0.9$, $r_M=1.1$, $\alpha_1=\epsilon_1=0.005$, $\alpha_2=\epsilon_2=0.03$, $\alpha_3=\epsilon_3=0.3$. The number of outer iterations necessary for convergence for Reynolds numbers 10 and 100 were 67 and 31. Convergence for Reynolds number 1000 was achieved in 22 outer iterations by modifying $H_1^{(0)}$ and $M_1^{(0)}$ to agree with

(3.3)
$$H^{0}(z) = \begin{cases} (-1.2)z & , & 0 \le z \le \frac{1}{4} \\ -0.3 + (1.2)(z - \frac{1}{4}), & \frac{1}{4} \le z \le \frac{3}{4} \\ (-1.2)(z - 1) & , & \frac{3}{4} \le z \le 1 \end{cases}$$

(3.4)
$$M^{(0)}(z) = \begin{cases} -10 + 52z & , & 0 \le z \le \frac{1}{4} \\ 3 - 12(z - \frac{1}{4}), & \frac{1}{4} \le z \le \frac{3}{4} \\ 10 + 52(z - 1), & \frac{3}{4} \le z \le 1 \end{cases}$$

respectively, at the grid points.

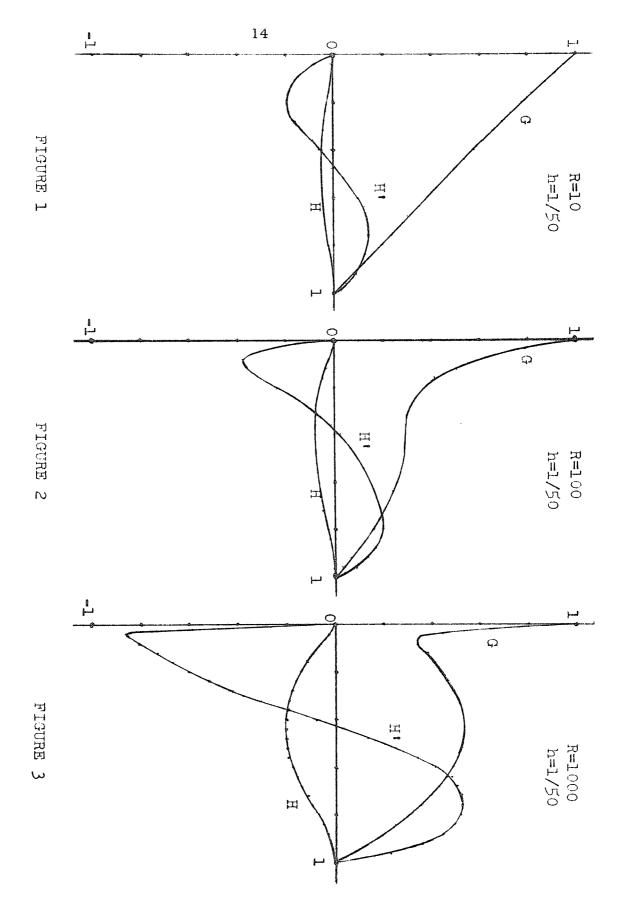
Finally, because of the broad interest in large Reynolds numbers and because the contradictary conclusions reached in certain cases of counter rotation, attention was turned to refined calculations for the case R = 2000, Ω_1 = 1, and Ω_2 = -1. In Figures 7 and 8 are shown the results for H, H', G, and M for the parameter choices h = 1/400, $\rho = 0.05$, $\mu = 0.05$, $\delta_1 = 0.1$, $\delta_2 = 0.925$, $r_H = 1.8$, $r_G = r_M = 0.8$, $\alpha_1 = 0.0003$, $\alpha_2 = 0.001$, $\alpha_3 = 0.002$, $\epsilon_1 = \epsilon_2 = 0.001$, $\epsilon_3 = 0.01$ and for initial functions (3.3) and (3.4). Convergence was achieved in 128 outer iteration, which required seven minutes of running time. The increase in precision is readily apparent by comparing Figures 6 and 7. Moreover, since Figure 7 shows clearly that the fluid has separated into two distinct parts which rotate with relatively large, but with opposite, angular velocities, it is concluded the numerical solution supports Batchelor in the Batchelor-Stewartson controversy ([2], [20], [22]).

With regard to the computations by other methods, only the work of Pearson and that of Lance and Rogers appear to be numerically

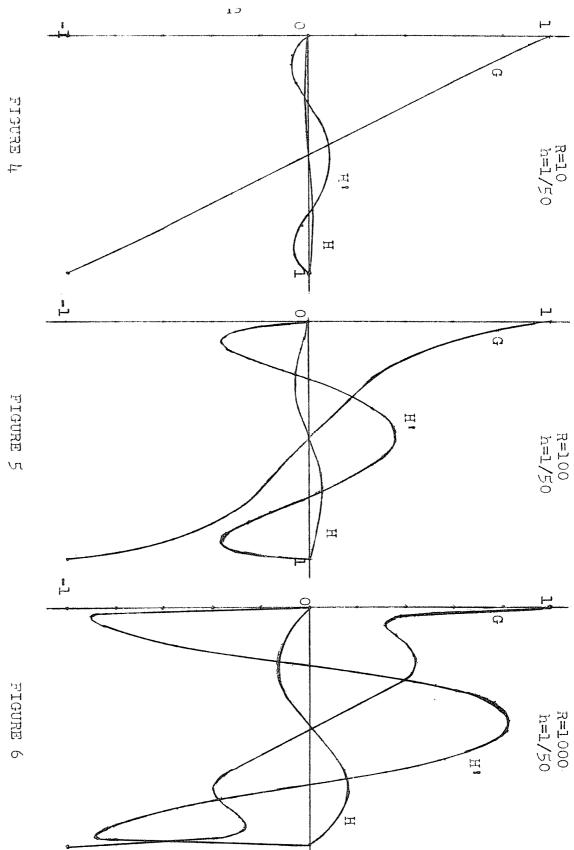
rigorous and moderately successful. For $R \le 100$, their results and ours for the case of a single rotating disk are completely comparable. Thereafter, various results differ widely. For example, for R = 1000, Ω_1 = 1 and Ω_2 = -1, Pearson produced two, distinct solutions but failed to produce the symmetric one. By relaxing the convergence tolerances, we too were able to produce more than one solution. However, sharpening these tolerances always resulted in one and only one solution. It is also rather interesting to observe that if, for Pearson's results (see [15], p. 632, Figure 9), the points where G and H cross the z axis are relocated to $z = \frac{1}{2}$, while the points where $H_{\overline{z}}$ crosses the z axis are relocated symmetrically about $z = \frac{1}{2}$, then the resulting configurations for G, H and H_z are qualitatively analogous to those shown in our Figure 7. One can only surmize, then, that Pearson's time dependent calculations are stable, but relatively inaccurate due to an accumulation of roundoff error. Such types of calculations are very common in the study of nonlinear problems.

In the study of R = 1023, Ω_1 = 1, Ω_2 = -1, Lance and Rogers assumed symmetry and reformulated the problem on the half interval $0 \le z \le \frac{1}{2}$. All their previous calculations were limited to R \le 529, but the use of symmetry allowed for a decrease in grid size and a corresponding increase in Reynolds number. Their results (see [12],

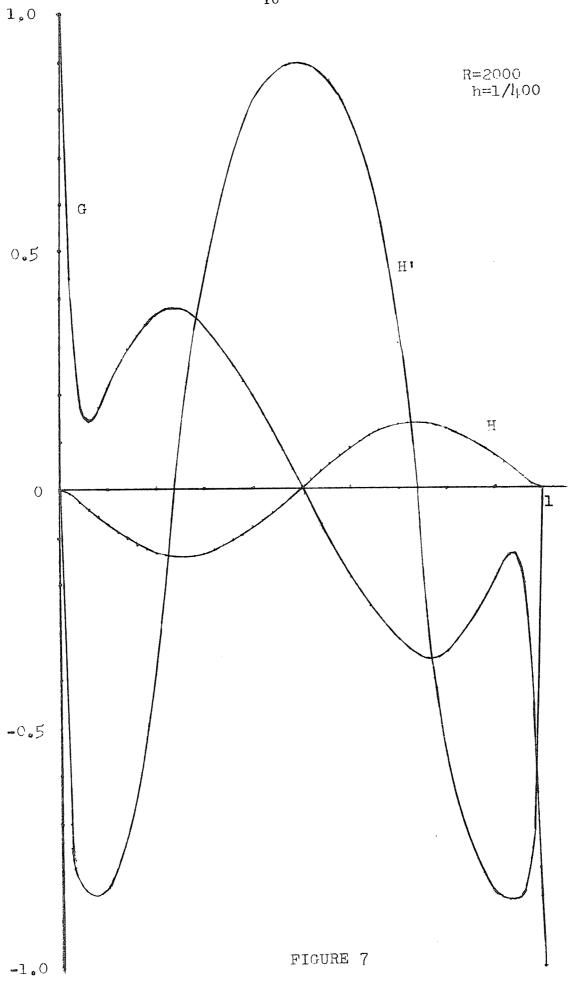
pp. 119-120) show that the main body of the fluid is only slightly disturbed, thus contradicting the flow shown in our Figure 7, and thereby supporting Stewartson in the Batchelor-Stewartson controversy. However, Lance and Rogers failed to demonstrate that the problem they study on the interval $0 \le z \le \frac{1}{2}$ is, in fact, equivalent to the given problem (1.2)-(1.7) of counter rotating disks. Indeed, numerically, they should have required that the differential equations be satisfied on $z = \frac{1}{2}$, which they failed to do ([12], p. 119, eq. 5.8). Indeed, since the solution shown in our Figure 7 also satisfies the conditions (5.8) of [12], the Lance and Rogers formulation has at least two solutions, namely theirs and ours, and appears to be a weaker problem than the one originally posed. The question as to whether or not the Lance and Rogers solution satisfies the differential equations on $z = \frac{1}{2}$ does not, however, appear to be trivial.











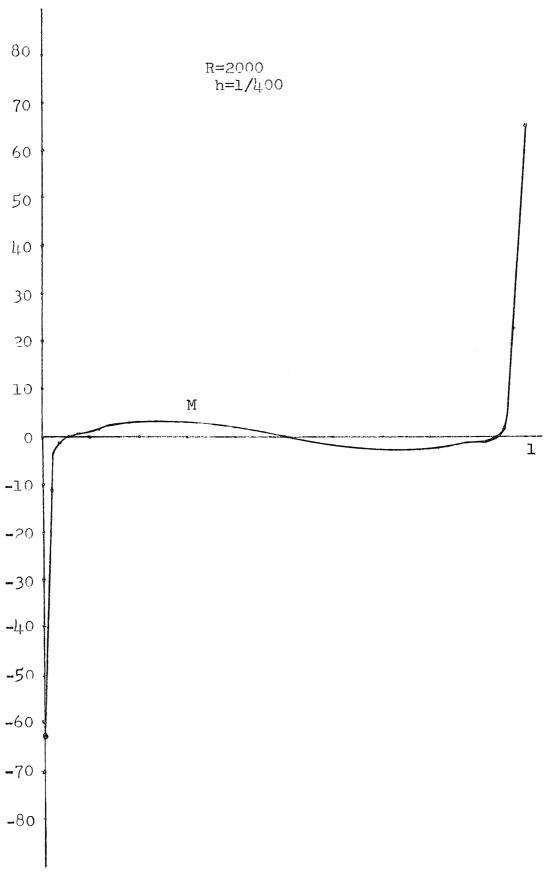


FIGURE 8

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```
1 0
            PARAMETER NMAX=401
2 *
            REAL MU.M(NMAX, 3), MO(NMAX)
            DIMENSION OMEGA( 2) . H(NMAX . 3) . G(NMAX . 3) . DXSQM(NMAX) . BO(NMAX) .
30
40
              B1(NMAX),B2(NMAX),CG(NMAX),CM(NMAX),DELTA(2),HPR(NMAX)
5 .
            DIMENSION HO (NMAX), GO (NMAX)
64
            COMMON H.G.M
70
            COMMON/ITOUT/ITOUT/NP1/NP1/NTH,NTG,NTM/INCPR/INCPR
8 8
            COMMON/CON/BO.B1.B2.CG.CM/DXSQ/DXSQ/N/N/NM1/NM1/R/R
90
            DATA MAXIT, MAXOUT/800, 200/, IBUG, INCOUT/1, 1/, INCSOR, INCRES/801, 200/
100
            DATA INSW/D/, INCPR/4/
         99 FORMAT(11E5.5)
110
         98 FORMATIOSOR ITERATION FOR H FAILED IN OUTER ITERATION 15.
124
13 *
               " GO TO NEXT PARAMETER CASE ")
140
         97 FORMAT( ODSOR ITERATION FOR G FAILED IN OUTER ITERATION 15,
15#
           . . GO TO NEXT PARAMETER CASE. .)
         96 FORMAY( OSOR ITERATION FOR M FAILED IN OUTER ITERATION ! 15.
160
17#
           * ° GO TO NEXT PARAMETER CASE . °)
         95 FORMATI OUTER ITERATION FAILED AFTER MAX. NO. OF ITERATIONS. PROC
180
194
           *EED TO NEXT PARAMETER CASE. *)
20*
         94 FORMAT (1H1 °DX = F7.5,5X OMEGA(1) = F5.2,5X OMEGA(2) = F5.2.
           * 5% PREYNOLDS NO. = PF7.0/1HO3% SMOOTHING SX POVER-RELAX. PSX
210
            OCONVERGENCE 1/5X 1FACTOR 9X 1FACTOR 9X 1TOLERANCE 1
220
23*
            * 6X "SOR TOLERANCE"/ 1HO 1X 1HH
240
           4F6.3.F16.3.ZF17.4/2X1HGF6.3.F16.3.ZF17.4/2X1HM2F6.3.F10.3.ZF17.4)
250
         93 FORMAT ( OCONVERGENCE ATTAINED. TOTAL SOR ITERATIONS FOR H. G. M = 9
           # 317)
260
270
         92 FORMAT (OUTOTAL SOR ITERATIONS FOR H.G.M # 317)
280
         90 FORMAT(1x F9.3,3F8.3,14F7.3)
290
         89 FORMAT(1H )
300
         88 FORMAT (OH AT SOR ITERATION 16)
310
        188 FORMAY (OG AT SOR ITERATION 16)
        288 FORMAT( OM AT SOR ITERATION 16)
32 *
330
         87 FORMAY ("OH-PRIME")
34#
         84 FORMAT (13F6.3)
         83 FORMAT("OH, G, M INITIALLY"/)
35 e
360
             READ INPUT PARAMETERS
37 *
             IF (INSW.NE.1) GO TO 4
380
             READ(5,84) (HD(I), I=1, NMAX)
390
             READ (5,84) (GO(1), I=1, NMAX)
400
             READ(5,84) (MO(1),1=1,NMAX)
410
           4 READ(5,99) ESH, ESG, ESM, FIN2
           5 READ(5,99) DX, OMEGA, R, EH, EG, EM, FIN
420
430
           7 READ(5.99) RHO, MU, DELTA, RH, RG, RM, END
440
             WRITE(6,94) DX, OMEGA, R, RHO, RH, EH, ESH, MU, RG, EG, ESG, DEL TA, RM, EM, ESM
450
             N=1 0/DX 0005
460
             NP1=N+1
470
             NM I = N = I
480
             INITIALIZE FUNCTIONS FOR OUTER ITERATION
      C
490
      Ç
500
             IF (INSW. EQ. 1) GO TO 11
51#
             DO 10 1=1, NP1
52*
             X=FLOAT(I-1) DX
53*
             G(1,3)=(OMEGA(2)=OMEGA(1)) + X + OMEGA(1)
```

```
IF (X . GT . . 25) GO TO 8
540
              H(1,3)==1,20X
55°
560
              M(1,3)=52.9X=10.
570
              GO TO 10
            8 IF (X.GT. .75) GO TO 9
580
590
              H(1,3)=1,20X=,6
              M(103)==1200X+60
600
              GO TO 10
610
620
            9 H(1,3)==1,2=X+1,2
              M(1,3)=52.4\times42.
630
640
           10 CONTINUE
              GO TO 211
650
           11 DO 111 I=1, NP1
660
              H(1.3)=HO(1)
670
689
              G(1,3) = GO(1)
690
          111 M(103)=MO(1)
          211 DO 12 J=1.2
700
710
              H(1,J)=H(1,3)
720
              H(NP1, J)=H(NP1, 3)
              M(1,J) = M(1,3)
734
740
              M(NP1,J)=M(NP1,3)
750
              G(1,J)=G(1,3)
760
           12 G(NP1, J) = G(NP1, 3)
770
              WRITE(6,83)
780
              WRIYE(6,90) (H([,3), I=1, NP1, INCPR)
              WRITE(6,90) (G(1,3), I=1, NP1, INCPR)
790
              WRITE(6,90) (M(1,3), 1=1, NP1, INCPR)
80 *
              DXSQ=DX++2
810
820
              AH1=1.0RH
              AH2=RH/2.
830
840
              RDXSReDX
              AG1=1 .- RG
85°
 860
              AM1=1 .- RM
 87 4
              HSQ2=2./DXSQ
 88
              NTOTHED
              NTOTGED
89#
900
              NTOTMED
 910
              ITOUTED
 920
           16 ITOUT = ITOUT + I
              DO 17 1=2.N
 934
 940
              H(1,1)=H(1,3)
              G(I_0I) = G(I_03)
 954
 960
           17 M(101) = M(103)
 970
              M(l_0 l) = M(l_0 3)
 98#
              M(NPl_{p}l)=M(NPl_{q}3)
               SOLVE FOR H-BAR BY SOR ITERATION
 990
1000
               NTHOO
101*
               DO 18 1=2.N
1020
           18 DXSQM(I)=DXSQ@M(I,1)
           20 NTHONTHOL
1030
1040
               DO 22 1=2,N
1050
           22 H(1,2) = H(1,3)
               H(2,3)=AH1@H(2,2)@RH/4.@H(3,2)
1060
107#
               DO 25 1=3,NM1
           25 H(Io3) = AH1+H(Io2) + AH2+(H(I+1o3) + H(I+1o2) = DX5QM(I))
1080
1090
               H(No3) = AH1 + H(No2) + RH/4 + + H(NM1,3)
1100
               TEST FOR CONVERGENCE
```

```
1119
              DO 27 1=2,N
1120
              IF ( ONOT O (ABS (H(102) +H(103)) OLT O ESH)) GO TO 33
1130
           27 CONTINUE
1140
       C
              CONVERGENCE ATTAINED -- SMOOTH SOLUTION
1150
              DO 30 1 = 2 . N
           3^{\circ} H(1,3)=RHO+H(1,3)+(1,=RHO)+H(1,1)
1160
1174
              GO TO 34
1180
       C
              CONVERGENCE UNATTAINED -- UPDATE FOR NEXT ITERATION UNLESS ITERATION
1194
       C
             LIMIT HAS BEEN EXCEEDED.
1200
           33 IF (MOD (NTH, INCSOR) NE O ) GO TO 133
121#
              WRITE (6,88) NTH
1220
              WRITE(6,90) (H(1,3), 1=1,NP1,1NCPR)
1230
          133 IF (NTHOLTOMAXIT) GO TO 20
1240
              WRITE(6,98) ITOUT
125#
              GO TO 62
       C
126#
              SOLVE FOR G-BAR BY SOR ITERATION
127#
           34 DO 35 1=2.N
128
              BO(1)=-2.0RDX@ABS(H(1,3))
1290
              BI(I)=(10+RDX+AMAX1(000H(1,3)))
130 *
              B2(1)=(10=RDX*AMIN1(000H(103)))
1310
           35 CG([]==0.50RDX0G([,1)0(H([+1,3)-H([-1,3))
1320
              NTGOD
1330
           36 NTG=NTG+1
1340
              DO 37 1=2.N
1350
              G(1,2)=G(1,3)
1360
              DO 38 1=2.N
1370
           38 G([,3)=AG1@G([,2]=RG@(B]([)@G([=1,3)@B2([)@G([+1,2)@CG([)]/BD([)
1380
              TEST FOR CONVERGENCE
1390
              DO 40 1=2.N
1400
              IF ( . NOT . (ABS (G ( I . 2) = G ( I . 3 ) ) . LT . ESG ) ) GO TO 44
1410
           40 CONTINUE
1420
       C
              CONVERGENCE ATTAINED - SMOOTH SOLUTION
1430
              DO 42 1=2,N
1440
           42 G(1,3)=MU*G(1,3)+(1,0-MU)*G(1,1)
1450
              GO TO 46
1460
              CONVERGENCE UNATTAINED -- UPDATE FOR NEXT SOR ITERATION UNLESS
       C
1470
              MAX. ITERATION LIMIT HAS BEEN EXCEEDED.
           44 IF (MOD (NTG , INCSOR) , NE , D) GO TO 144
1480
1490
              WRITE (6, 188) NTG
1500
              WRITE(6,90) (G(1,3), I=1, NP1, INCPR)
151
          144 IF (NTG.LT. MAXIT) GO TO 36
1520
              WRITE(6,97) ITOUT
153*
              GO TO 62
1540
       C
              COMPUTE MEBAR AT BOUNDARY POINTS
155
           46 M(1.3)=DELTA(1)+HSQ2+H(2.3)+(1.*DELTA(1))+M(1.1)
1560
              M(NP1,3)=DELTA(1) + SQ2+H(N,3)+(1++DELTA(1)) + M(NP1,1)
157
       C
              SOLVE FOR M-BAR AT INTERIOR POINTS
158
              DO 48 1=2 N
1590
           48 CM(1)=200RDX+G(103)+(G(1+103)-G(1-103))
1600
              M(NP1,2)=M(NP1,3)
1610
          148 NTM 0
162"
           49 NTM=NTM+1
163*
              DO 50 1=2.N
1645
           50 M(1,2)=M(1,3)
1650
              DO 52 1=2,N
1660
           52 M(I,3)=AM1+M(I,2)-RM+(B1(I)+M(I+1,3)+B2(I)+M(I+1,2)+CM(I))/BO(I)
1679
              TEST FOR CONVERGENCE
```

168				
169°	1680			DO 54 1=2.N
170				
1710 C CONVERGENCE ATTAINEDSMOOTH SOLUTION DO 55 12,N S S 12,N S S 12,N S S 12,N S S S S S S S S S			54	
172° DO 55 1-2, N 5 M(1,3) + (1,-DELTA(2)) + M(1,1) 174° GO TO 58 175° C CONVERGENCE UNATTAINED + WEDDATE FOR NEXT SOR TERATION UNLESS 176° C CONVERGENCE UNATTAINED + WEST SOR TERATION UNLESS 176° C CONVERGENCE UNATTAINED + WEST SOR TERATION UNLESS 176° C CONVERGENCE UNATTAINED + WEST SOR TERATION UNLESS 176° MRITE(6,90) (M(1,3),1=1,NP1,1NP1,1NPCR) 180° S F F F MINTALT GO TO 49 181° WRITE(6,90) TOUT 182° GO TO 62 183° S F F MOD(ITOUT, INCORD) CALL OUTPUT 184° IF MOD(ITOUT, INCORD) CALL OUTPUT 186° NTOTH-NTOTH-NTH 186° NTOTH-NTOTH-NTH 186° NTOTH-NTOTH-NTH 187° IF MOD(ITOUT, INCORD) CALL SET 187° MINTAINED MOD SOR MOD SOR 190° F F MOD SOR MOD SOR 190° F MOD SOR MOD SOR 191° IF MOD SOR MOD SOR MOD SOR 193° S CONTINUE 194° IF MOD SOR MOD SOR MOD SOR 196° C CONVERGENCE ATTAINED + OUTPUT SOLUTION 197° IF MOD SOR MOD SOR MOD SOR 198° C CONVERGENCE ATTAINED + OUTPUT SOLUTION 198° C CONVERGENCE ATTAINED + OUTPUT SOLUTION 199° MRITE(6,87) MRITE(6,87) MRITE(6,87) MRITE(6,87) MRITE(6,87) MRITE(6		Ċ	<u>-</u>	CONVERGENCE ATTAINED SMOOTH SOLUTION
1730 55 M(1,3)=DELTA(2)=M(1,3)+(1DELTA(2)=M(1,1) 1740 CO		•		
175			55	
1750 C				GO 70 58
		C		CONVERGENCE UNATTAINED == UPDATE FOR NEXT SOR ITERATION UNLESS
1780	1760	C		STERATION LIMIT HAS BEEN EXCEEDED.
1990	1770		56	IF (MOD (NTM, INCSOR) NEOD) GO TO ST
180	1780			WRITE(6,288) NTM
1810	1790			WRITE(6,90) (M(I,3), I=1, NP1, INCPR)
182	1000		57	
183	1810			WRITE(6,96) ITOUT
184°	1820			GO TO 62
1850	1830		58	IF (MOD (ITOUT, INCOUT) . EQ. O) CALL OUTPUT
186°	1840			IF (MOD (ITOUT, INCRES) . EQ.O) CALL TEST
NTOTM=NTOTM+NTM	1850			NTOTH=NTOTH + NTH
188	1869			NTOTG=NTOTG+NTG
189°	1870			
1900	1880	C		TEST FOR CONVERGENCE OF OUTER ITERATION
1910	1890			
1920	1900			
1930	1910			
1940	1920			
1950	1930		59	
196				IF(ONOTO (ABS(M(1,3) = M(1,1)) OLTOEM))GO TO 60
1970	1950			
198° C		C		
199* DO 159 I=2,N 200* 159 HPR(I)=(H(I*1,3)=H(I*1,3))/(2.*DX) 201* WRITE(6,87) 202* WRITE(6,87) 203* IF(MOD(ITOUT,INCRES).NE.O) CALL TEST 204* WRIYE(6,93) NTOTH,NTOTG,NTOTM 205* GO TO 62 206* C CONVERGENCE UNATTAINED==OUTPUT VALUES FOR OUTER ITERATION AND 207* C UPDATE FOR NEXT OUTER ITERATION UNLESS OUTER ITERATION LIMIT 208* C HAS BEEN EXCEEDED. 209* 60 IF(ITOUT.LT.*MAXOUT) GO TO 16 210* WRITE(6,92) NTOTH,NTOTG,NTOTM 211* WRITE(6,95) 212* 62 IF(ABS(END).GT.O.) GO TO 63 213* GO TO 7 214* 63 IF(ABS(FIN).GT.O.) GO TO 64 215* GO TO 5 64 IF(ABS(FIN2).GT.O.) STOP 217* GO TO 4				
200° 159 HPR(I) = (H(I + 1, 3) = H(I = 1, 3))/(2.*DX) 201° WRITE(6.*87) 202° WRITE(6.*90) (HPR(I)), I = 1.NP1.INCPR) 203° IF (MOD(ITOUT.INCRES).NE.O) CALL TEST 204° WRIYE(6.*93) NTOTH.NTOTG.NTOTM 205° GO TO 62 206° C CONVERGENCE UNATTAINED==OUTPUT VALUES FOR OUTER ITERATION AND 207° C UPDATE FOR NEXT OUTER ITERATION UNLESS OUTER ITERATION LIMIT 208° C HAS BEEN EXCEEDED. 209° 60 IF (ITOUT.LT.MAXOUT) GO TO 16 210° WRITE(6.*92) NTOTH.NTOTG.NTOTM 211° WRITE(6.*95) 212° 62 IF (ABS(END).GT.O.) GO TO 63 213° GO TO 7 214° 63 IF (ABS(FIN).GT.O.) GO TO 64 215° GO TO 5 216° 64 IF (ABS(FIN2).GT.O.) STOP 217° GO TO 4		C		
201 WRITE(6,87) 202 WRITE(6,90) (HPR(I),Im 1,NPI,INCPR) 203 IF(MOD(ITOUT,INCRES).NE.O) CALL TEST 204 WRITE(6,93) NTOTH,NTOTG,NTOTM 205 GO TO 62 206 C CONVERGENCE UNATTAINED=OUTPUT VALUES FOR OUTER ITERATION AND 207 C UPDATE FOR NEXT OUTER ITERATION UNLESS OUTER ITERATION LIMIT 208 C HAS BEEN EXCEEDED. 209 60 IF(ITOUT.LT.MAXOUT) GO TO 16 210 WRITE(6,92) NTOTH,NTOTG,NTOTM 211 WRITE(6,95) 212 62 IF(ABS(END).GT.O.) GO TO 63 213 GO TO 7 214 63 IF(ABS(FIN).GT.O.) GO TO 64 215 GO TO 5 216 64 IF(ABS(FIN2).GT.O.) STOP 217 GO TO 4			_	
202* WRITE(6,90) (HPR(I),I= 1,NPI,INCPR) 203* IF(MOD(ITOUT,INCRES),NE.O) CALL TEST 204* WRIYE(6,93) NYOTH,NYOTG,NTOTM 205* GO TO 62 206* C CONVERGENCE UNATTAINED=OUTPUT VALUES FOR OUTER ITERATION AND 207* C UPDATE FOR NEXT OUTER ITERATION UNLESS OUTER ITERATION LIMIT 208* C HAS BEEN EXCEEDED. 209* 60 IF(ITOUT,LT,MAXOUT) GO TO 16 210* WRITE(6,95) 212* G2 IF(ABS(END),GT,O,) GO TO 63 213* GO TO 7 214* G3 IF(ABS(FIN),GT,O,) GO TO 64 215* GO TO 5 216* 64 IF(ABS(FIN2),GT,O,) STOP 217* GO TO 4	-		159	
IF (MOD (ITOUT, INCRES).NE.O) CALL TEST 204* WRITE (6.93) NTOTH, NTOTG, NTOTM 205* GO TO 62 206* C CONVERGENCE UNATTAINED OUTPUT VALUES FOR OUTER ITERATION AND 207* C UPDATE FOR NEXT OUTER ITERATION UNLESS OUTER ITERATION LIMIT 208* C HAS BEEN EXCEEDED. 209* 60 IF (ITOUT.LT.MAXOUT) GO TO 16 210* WRITE (6.92) NTOTH, NTOTG, NTOTM 211* WRITE (6.95) 212* 62 IF (ABS(END).GT.O.) GO TO 63 213* GO TO 7 214* 63 IF (ABS(FIN).GT.O.) GO TO 64 215* GO TO 5 216* 64 IF (ABS(FIN2).GT.O.) STOP 217* GO TO 4				
### WRITE(6,93) NTOTH.NTOTG.NTOTM #### 205* GO TO 62 #### 206* C CONVERGENCE UNATTAINED OUTPUT VALUES FOR OUTER ITERATION AND ###################################				
GO TO 62 206				
CONVERGENCE UNATTAINED == OUTPUT VALUES FOR OUTER ITERATION AND UPDATE FOR NEXT OUTER ITERATION UNLESS OUTER ITERATION LIMIT HAS BEEN EXCEEDED. OF A STANDARD STORM S				
2070 C UPDATE FOR NEXT OUTER ITERATION UNLESS OUTER ITERATION LIMIT 2080 C HAS BEEN EXCEEDED. 2090 60 IF (ITOUT.LT.MAXOUT) GO TO 16 2100 WRITE (6,92) NTOTH, NTOTG, NTOTM 2110 WRITE (6,95) 2120 62 IF (ABS(END).GT.O.) GO TO 63 2130 GO TO 7 2140 63 IF (ABS(FIN).GT.O.) GO TO 64 2150 GO TO 5 2160 64 IF (ABS(FIN2).GT.O.) STOP 2170 GO TO 4		_		CONVERCENCE HARRIANED ROLLERING VALUES FOR OUTER TRERATION AND
208		-		LUNVERGENCE UNATTAINED TOOL VALUES FOR VOIER TERATION LIMIT
209		_		
210° WRITE(6,92) NTOTH,NTOTG,NTOTM 211° WRITE(6,95) 212° 62 IF(ABS(END)°GT°D°) GO TO 63 213° GO TO 7 214° 63 IF(ABS(FIN)°GT°D°) GO TO 64 215° GO TO 5 216° 64 IF(ABS(FIN2)°GT°D°) STOP 217° GO TO 4		C	, n	
211° WRITE(6,95) 212° 62 IF(ABS(END)°GT°D°) GO TO 63 213° GO TO 7 214° 63 IF(ABS(FIN)°GT°D°) GO TO 64 215° GO TO 5 216° 64 IF(ABS(FIN2)°GT°D°) STOP 217° GO TO 4			- 60	
212 62 IF (ABS(END) • GT • D •) GO TO 63 213 GO TO 7 214 63 IF (ABS(FIN) • GT • D •) GO TO 64 215 GO TO 5 216 64 IF (ABS(FIN2) • GT • D •) STOP 217 GO TO 4	-			
213 GO TO 7 214 63 IF(ABS(FIN) • GT • D •) GO TO 64 215 GO TO 5 216 64 IF(ABS(FIN2) • GT • D •) STOP 217 GO TO 4			, າ	
214° 63 IF(ABS(FIN)°GT°D°) GO TO 64 215° GO TO 5 216° 64 IF(ABS(FIN2)°GT°D°) STOP 217° GO TO 4			6 £	
215* GO TO 5 216* 64 IF(ABS(FIN2).GT.D.) STOP 217* GO TO 4			, 2	·
2160 64 IF (ABS (FIN2) o GT o D o) STOP 2170 GO TO 4	-		63	
217 GO TO 4			n	
			67	
6 10 V ENV				
	~ 10 ~			E N V