

NUMERICAL SOLUTION OF A CLASS OF  
NONSTEADY CAVITY FLOW PROBLEMS

by Donald Greenspan

APPENDIX: PROGRAMMING VISCOUS  
INCOMPRESSIBLE FLOW PROBLEMS

by David Schultz

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## 1. INTRODUCTION.

In recent years a large variety of viscous flow problems have been studied with the aid of modern, high speed digital computers (see, e.g., references [1] - [9] and the additional references contained therein). Those problems which are time dependent are usually treated by initial-value, or step-ahead, techniques, while those which are steady state are usually treated by boundary value techniques. But because step-ahead methods always contain an accumulation with time of both round-off and truncation errors, while boundary value methods tend to smooth out such errors, we will show in this paper how to apply a boundary value technique to a large class of prototype, time dependent problems.

## 2. THE ANALYTICAL PROBLEMS.

We will consider two-dimensional, incompressible flow problems in a cavity, which for simplicity will be taken to be a unit square. Analytically we seek to find two functions  $\psi(x, y, t)$  and  $\omega(x, y, t)$ ,  $0 \leq x \leq 1$ ,

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$0 \leq y \leq 1$ ,  $0 \leq t$  such that for a given non-negative number  $\mathcal{R}$  the following are valid:

$$(2.1) \quad \Delta\psi \equiv \frac{\partial^2\psi}{\partial x^2} + \frac{\partial^2\psi}{\partial y^2} = -\omega; \quad 0 < x < 1, \quad 0 < y < 1, \quad 0 < t$$

$$(2.2) \quad \frac{\partial\omega}{\partial t} = \frac{1}{\mathcal{R}} \Delta\omega + \frac{\partial\psi}{\partial x} \frac{\partial\omega}{\partial y} - \frac{\partial\psi}{\partial y} \frac{\partial\omega}{\partial x}; \quad 0 < x < 1, \quad 0 < y < 1, \quad 0 < t$$

$$(2.3) \quad \psi(x, y, 0) = \omega(x, y, 0) = 0; \quad 0 \leq x \leq 1, \quad 0 \leq y \leq 1$$

$$(2.4) \quad \psi(x, 0, t) = \frac{\partial\psi(x, 0, t)}{\partial y} = 0; \quad 0 \leq x \leq 1, \quad 0 \leq t$$

$$(2.5) \quad \psi(0, y, t) = \frac{\partial\psi(0, y, t)}{\partial x} = \psi(1, y, t) = \frac{\partial\psi(1, y, t)}{\partial x} = 0; \quad 0 \leq y \leq 1, \quad 0 \leq t$$

and

$$(2.6) \quad \psi(x, 1, t) = 0, \quad \frac{\partial\psi}{\partial y}(x, 1, t) = -1; \quad 0 \leq x \leq 1, \quad 0 \leq t.$$

In initial value problem (2.1) - (2.6),  $\psi$  is the stream function,  $\omega$  is the vorticity and  $\mathcal{R}$  is the Reynolds number. We will consider (2.1) - (2.6) under the assumption that a steady state solution exists and proceed numerically to show how the **nonsteady** flow can be reconstructed from the steady one.

### 3. THE NUMERICAL METHOD.

In this section, let us describe in complete generality a finite difference method for solving (2.1) - (2.6) numerically on a digital computer. Specific examples will be presented in Section 4.

The first step in the method is to solve numerically with grid size  $h$  the steady state problem associated with (2.1) - (2.6), and shown in Figure 3.1, in any of the presently available ways (for small  $\mathcal{R}$ , see [3] and [5]; for large  $\mathcal{R}$ , see [5]). This numerical solution will be denoted by  $\psi_h(x, y, \infty)$  and  $\omega_h(x, y, \infty)$ .

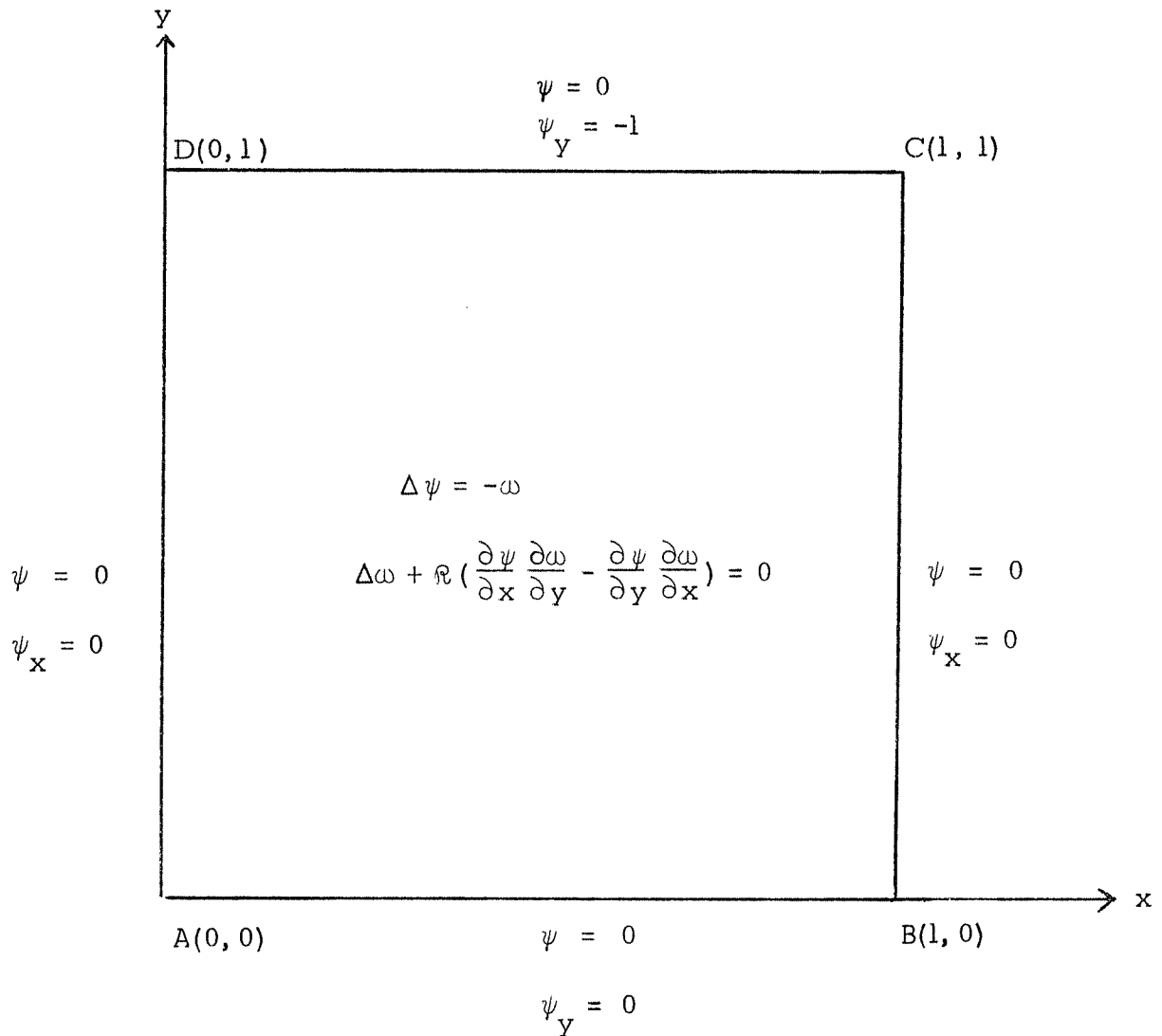


FIGURE 3.1

Next, for fixed  $t = T$ , subdivide  $0 \leq t \leq T$  into  $n$  equal parts, each of length  $\Delta t$ , by means of the points  $t_k = k\Delta t$ ;  $k = 0, 1, \dots, n$ , and, as shown in Figure 3.2, let  $P$  be the rectangular parallelepiped defined by  $P = \{(x, y, t): 0 \leq x \leq 1, 0 \leq y \leq 1, 0 \leq t \leq T\}$ . Define  $R$  to be the interior and  $S$  to be the boundary of  $P$ .

Using space grid size  $h$  and time grid size  $\Delta t$ , then construct in the usual way the three dimensional sets of interior grid points  $R_{h, \Delta t}$  and boundary grid points  $S_{h, \Delta t}$ . At the boundary grid points  $S_{h, \Delta t}$ , set

$$(3.1) \quad \psi(x, y, 0) = 0$$

$$(3.2) \quad \psi(x, y, T) = \psi(x, y, \infty)$$

$$(3.3) \quad \psi(0, y, t) = \psi(1, y, t) = \psi(x, 0, t) = \psi(x, 1, t) = 0.$$

At each point  $(x, y, t)$  of  $R_{h, \Delta t}$  define

$$(3.4) \quad \psi^{(0)}(x, y, t) = 0, \quad \omega^{(0)}(x, y, t) = 0.$$

We will now show how to construct from (3.4) on  $R_{h, \Delta t}$  a sequence of discrete functions

$$(3.5) \quad \psi^{(1)}, \psi^{(2)}, \psi^{(3)}, \dots, \psi^{(k)},$$

and on  $R_{h, \Delta t} + S_{h, \Delta t}$  a sequence of discrete functions

$$(3.6) \quad \omega^{(1)}, \omega^{(2)}, \omega^{(3)}, \dots, \omega^{(k)}$$

which will both converge. For this purpose, at each point of  $R_{h, \Delta t}$

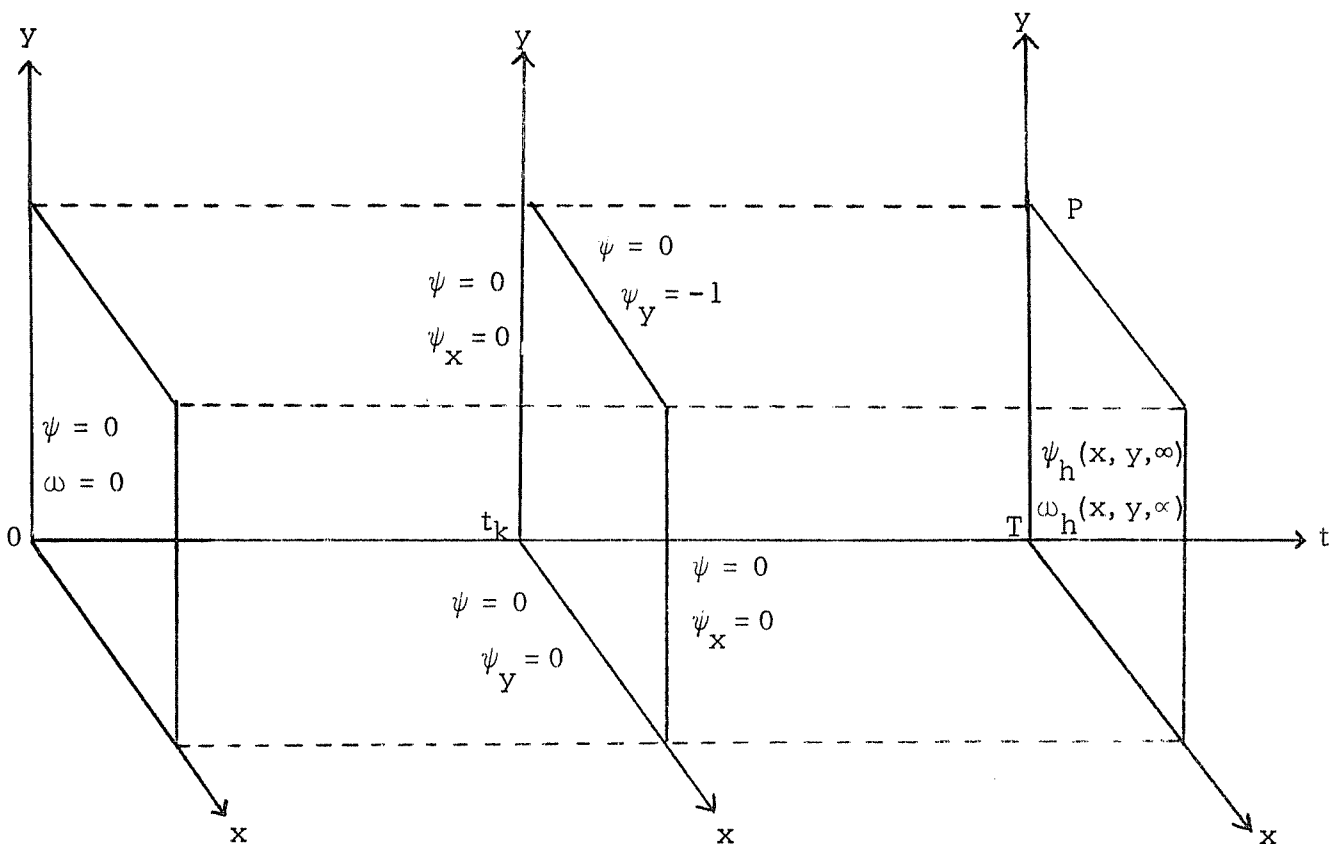


FIGURE 3.2

write down the difference equation

$$(3.7) \quad -4\psi(x, y, t_k) + \psi(x+h, y, t_k) + \psi(x, y+h, t_k) + \psi(x-h, y, t_k) \\ + \psi(x, y-h, t_k) = -h^2 \omega^{(0)}(x, y, t_k), \quad k = 1, 2, \dots, n-1.$$

Inserting the known values (3.1) - (3.3) wherever possible into (3.7), one then solves the resulting linear algebraic system by successive-over-relaxation with over-relaxation factor  $r_\psi$ . If the resulting solution is denoted by  $\bar{\psi}^{(1)}$ , then on  $R_{h,\Delta t}$  the element  $\psi^{(1)}$  of (3.5) is defined by

the smoothing formula

$$(3.8) \quad \psi^{(1)} = \rho\psi^{(0)} + (1 - \rho)\bar{\psi}^{(1)}, \quad 0 \leq \rho \leq 1.$$

Next, at each point of  $S_{h, \Delta t}$  set

$$(3.9) \quad \bar{\omega}^{(1)} = \frac{2\xi}{h} - \frac{2\psi^{(1)}}{h^2},$$

where  $\psi^{(1)}$  is evaluated at the point of  $R_{h, \Delta t}$  which is nearest to the given point and where

$$(3.10) \quad \xi = \begin{cases} 1, & \text{if } y = 1 \\ 0, & \text{if } y \neq 1. \end{cases}$$

At each point of  $R_{h, \Delta t}$ , write down the difference equation

$$(3.11) \quad \begin{aligned} & \frac{1}{2h} [-3\omega(x, y, t-\Delta t) + 4\omega(x, y, t) - \omega(x, y, t+\Delta t)] \\ & = \frac{1}{h^2\mathcal{R}} [-4\omega(x, y, t) + \omega(x+h, y, t) + \omega(x, y+h, t) \\ & \quad + \omega(x-h, y, t) + \omega(x, y-h, t)] + \alpha \cdot \beta - \gamma \cdot \delta, \end{aligned}$$

where

$$\alpha = \frac{\psi^{(1)}(x+h, y, t) - \psi^{(1)}(x-h, y, t)}{2h}$$

$$\gamma = \frac{\psi^{(1)}(x, y+h, t) - \psi^{(1)}(x, y-h, t)}{2h}$$

and



$$\beta = \frac{\omega(x, y+h, t) - \omega(x, y, t)}{h}, \quad \text{if } \alpha \geq 0$$

$$\beta = \frac{\omega(x, y, t) - \omega(x, y-h, t)}{h}, \quad \text{if } \alpha < 0$$

$$\delta = \frac{\omega(x, y, t) - \omega(x-h, y, t)}{h}, \quad \text{if } \gamma \geq 0$$

$$\delta = \frac{\omega(x+h, y, t) - \omega(x, y, t)}{h}, \quad \text{if } \gamma < 0.$$

Inserting the values (3.9) wherever possible into (3.11), one then solves the system generated by (3.11) by successive over-relaxation with over-relaxation factor  $r_\omega$ . The solution is denoted by  $\bar{\omega}^{(1)}$ . Then, on  $R_{h, \Delta t} + S_{h, \Delta t}$  one defines

$$\omega^{(1)} = \mu \omega^{(0)} + (1 - \mu) \bar{\omega}^{(1)}, \quad 0 \leq \mu \leq 1,$$

which completes the construction of the element  $\omega^{(1)}$  in sequence (3.6).

One proceeds next to construct  $\psi^{(2)}$  from  $\psi^{(1)}$  and  $\omega^{(1)}$  in the same spirit as  $\psi^{(1)}$  was constructed from  $\psi^{(0)}$  and  $\omega^{(0)}$ , and to generate  $\omega^{(2)}$  from  $\psi^{(2)}$  just as  $\omega^{(1)}$  was generated from  $\psi^{(1)}$ . And in the indicated fashion, the iteration continues until for some preassigned tolerance  $\epsilon$  one finds that uniformly

$$|\psi^{(k)} - \psi^{(k+1)}| < \epsilon$$

$$|\omega^{(k)} - \omega^{(k+1)}| < \epsilon.$$

The discrete functions  $\psi^{(k)}$  and  $\omega^{(k)}$  are then taken, on their points of definition, to be numerical approximations of  $\psi(x, y, t)$  and  $\omega(x, y, t)$ , respectively.

#### 4. EXAMPLES.

Various examples for  $0 \leq \mathcal{R} \leq 500$  were run on the CDC 3600 at the University of Wisconsin. Since all behaved similarly, we shall discuss in detail only the case  $\mathcal{R} = 500$ , with which other authors have found exceptional difficulties (see, e.g., [3]).

The steady state problem shown in Figure 3.1 was solved by the method in [5] for  $h = \frac{1}{20}$ . These results are shown graphically in Figures 4.1 and 4.2. Then, with  $T = 5$ ,  $\Delta t = \frac{1}{2}$ ,  $r_\psi = 1.8$ ,  $r_\omega = 1.0$ ,  $\rho = .3$ ,  $\mu = .7$  and  $\varepsilon = 10^{-3}$ , the method of Section 3 converged in 54 iterations, which took 22 minutes of running time. The stream curves  $\psi = .09, .07, .05, .03, .01$  and equivorticity curves  $\omega = 4, 1.6, 0$  are given for  $t = 1, 2, 3, 4$  in Figures 4.3 - 4.10.

It should be observed from this example that one gets excellent results for large time steps, which makes the method most attractive and exceptionally fast.

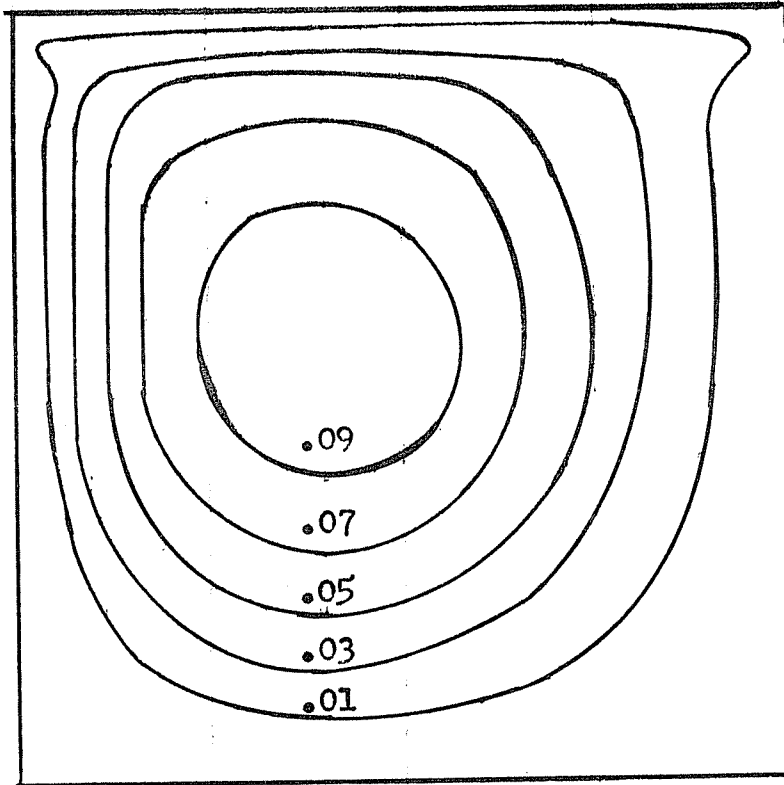


FIGURE 4.1 Steady state stream curves.

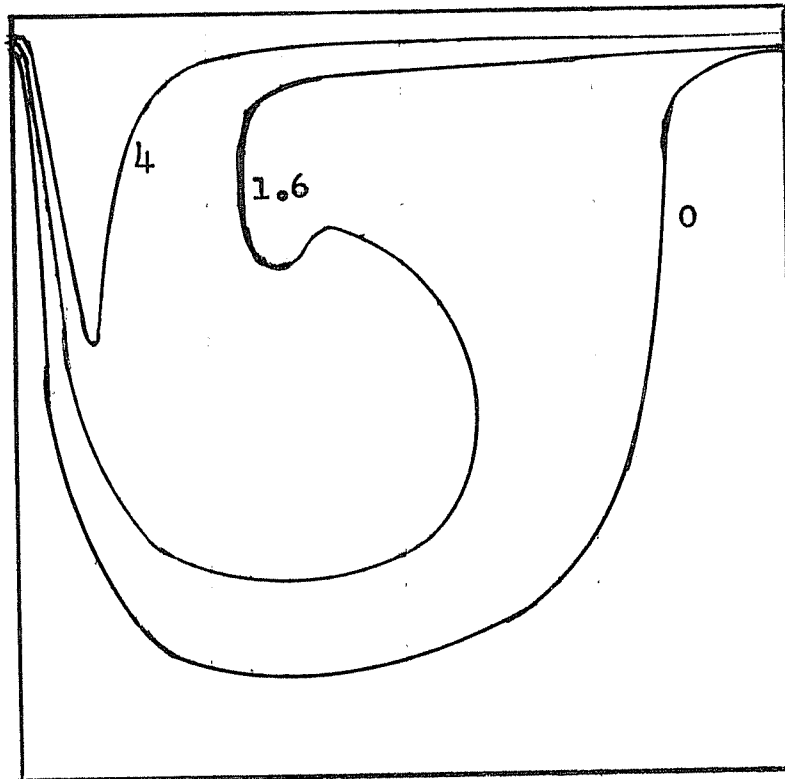
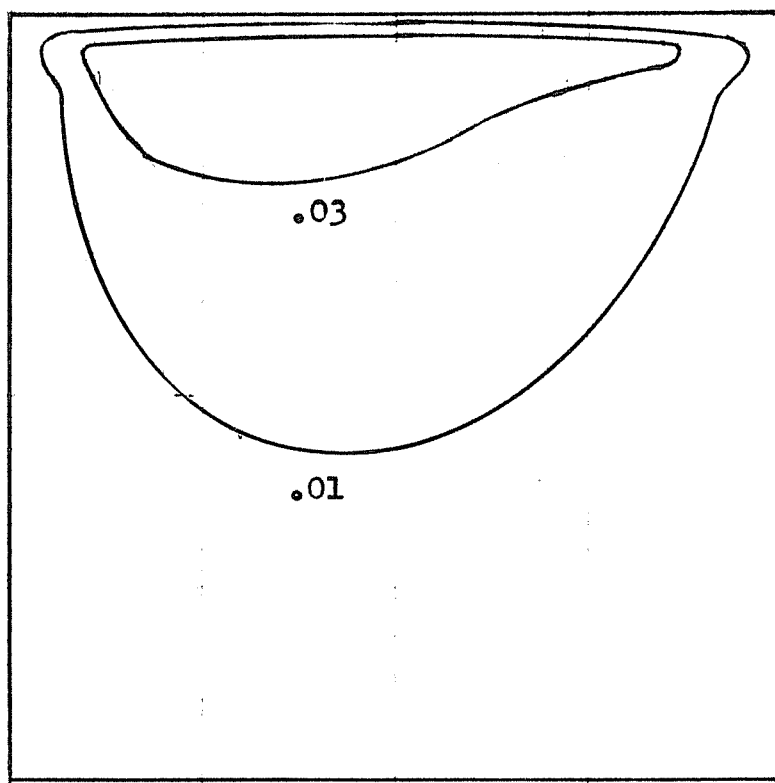
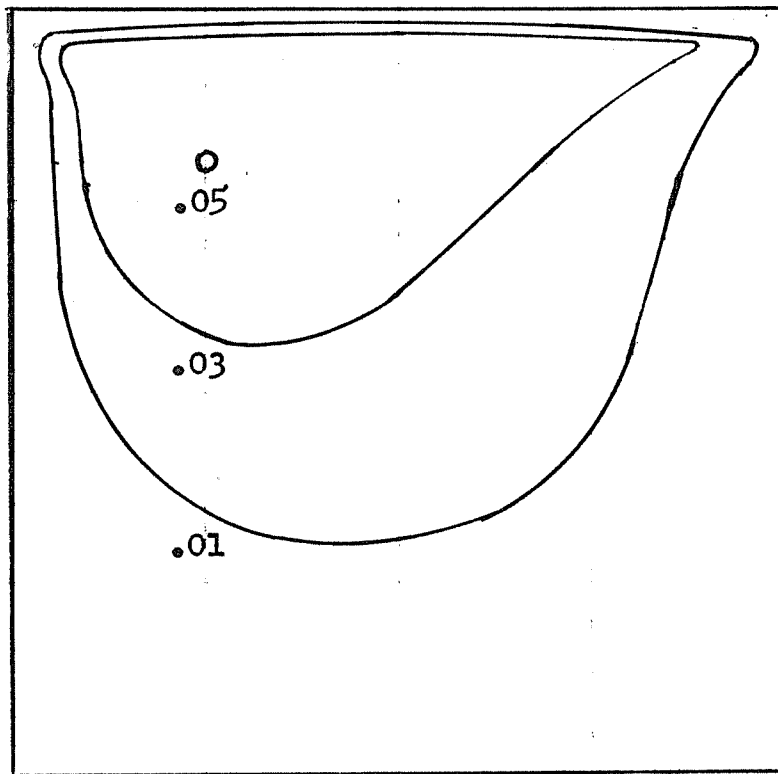


FIGURE 4.2 Steady state equivorticity curves.

FIGURE 4.3 Streamlines at  $t=1$ .FIGURE 4.4 Streamlines at  $t=2$ .

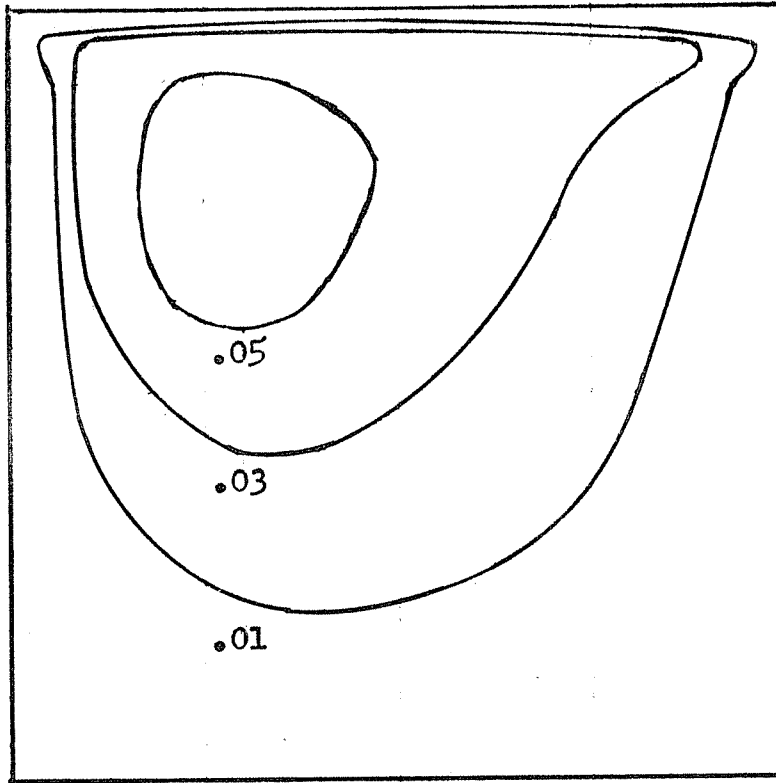


FIGURE 4.5 Streamlines at  $t=3$ .

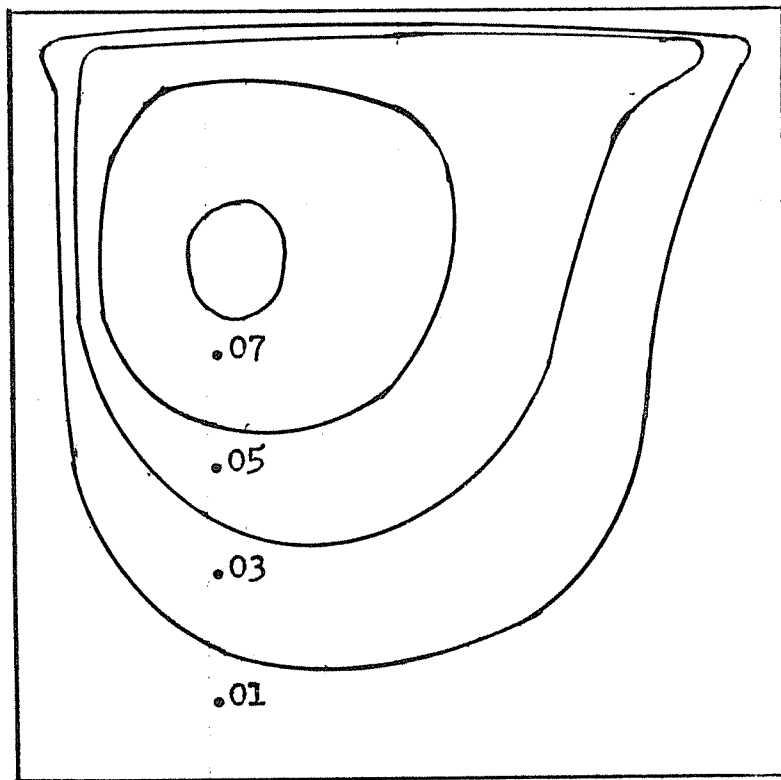


FIGURE 4.6 Streamlines at  $t=4$ .

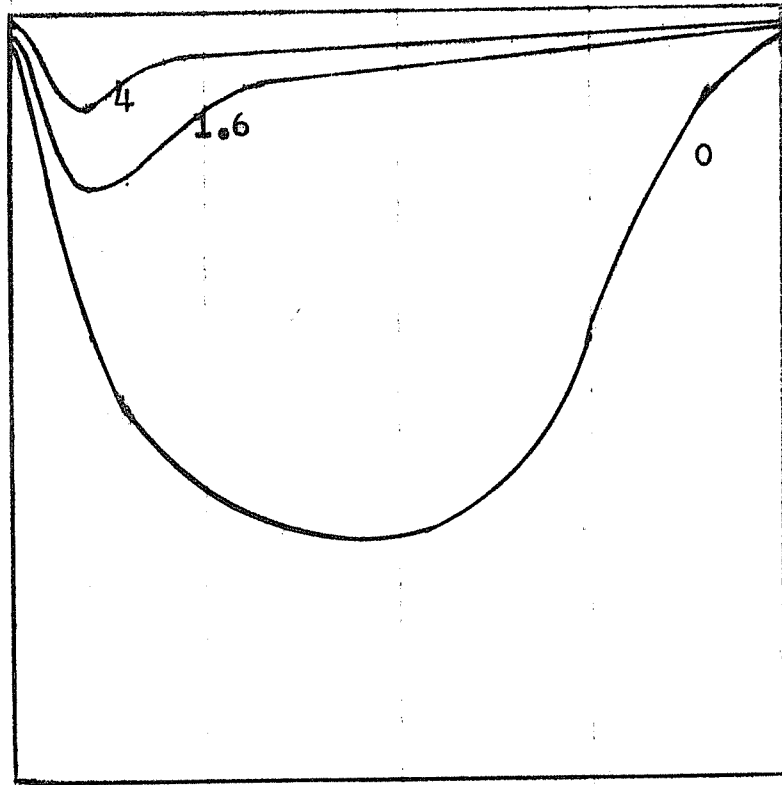


FIGURE 4.7 Equivorticity curves at  $t=1$ .

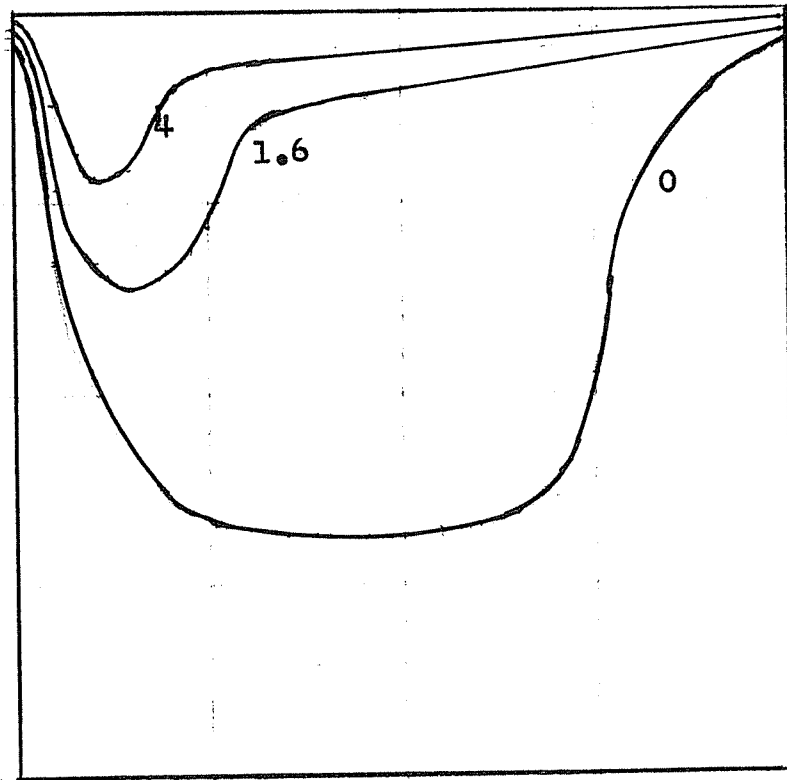


FIGURE 4.8 Equivorticity curves at  $t=2$ .

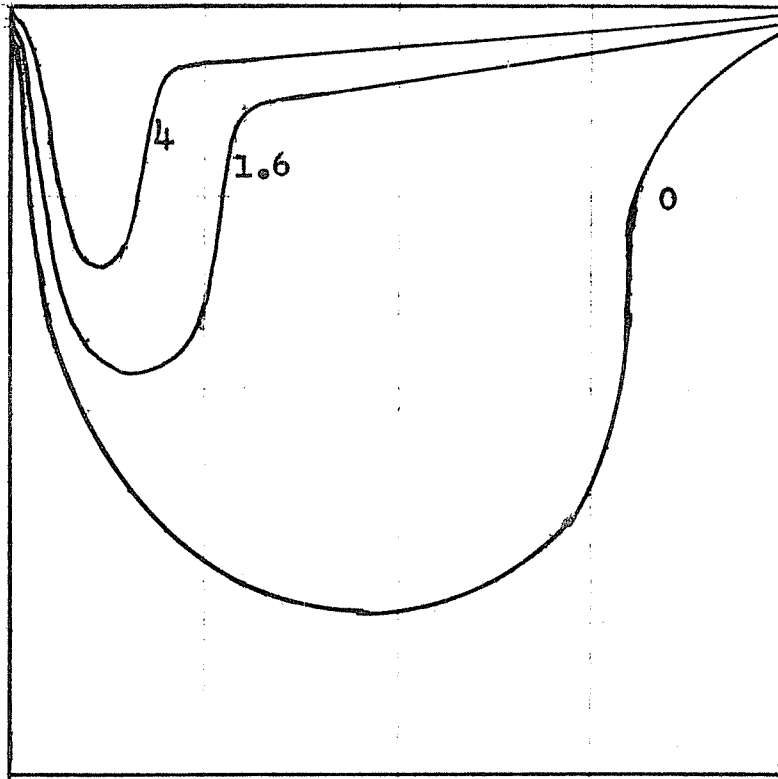


FIGURE 4.9 Equivorticity curves at  $t = 3$ .

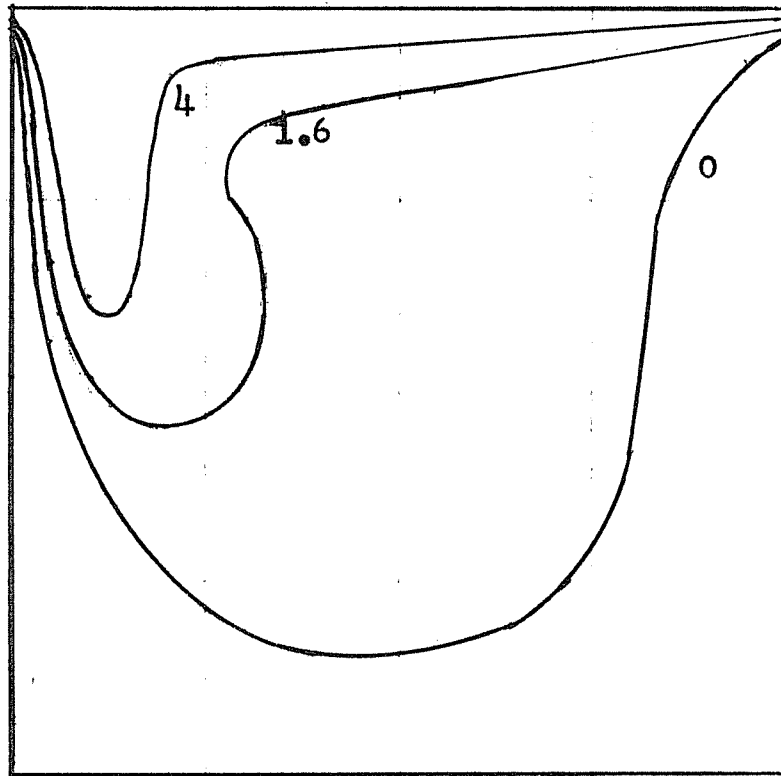


FIGURE 4.10 Equivorticity curves at  $t = 4$ .

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## APPENDIX

## PROGRAMMING VISCOUS, INCOMPRESSIBLE FLOW PROBLEMS

D. SCHULTZ

## DEFINITIONS OF PROGRAM VARIABLES

OMA = VORTICITY VALUES

PSI = STREAM VALUES

N = NUMBER OF VERTICAL SPACES IN THE GRID

M = NUMBER OF HORIZONTAL SPACES IN THE GRID

NT = NUMBER OF TIME STEPS

R = REYNOLD'S NUMBER

H = GRID SIZE

EPS = TOLERANCE FOR INNER-AND OUTER-ITERATIONS

C1 = WEIGHTING FACTOR FOR OMA

F1 = WEIGHTING FACTOR FOR PSI

RW = RELAXATION FACTOR FOR OMA EQUATIONS

NM = NUMBER OF OUTER-ITERATIONS

NCOUNT = NUMBER OF INNER-ITERATIONS

W0,W1,W2,W3,W4 = COEFFICIENTS FOR THE VORTICITY EQUATION

ISTOP = SWITCH TO INDICATE CONVERGENCE

```

PROGRAM NAVSTK
BANK,(0),NAVSTK,/2/
BANK,(1),/1/
COMMON/1/PSI(21,21,21),SVOUT(21,21,21),SVPSI(21,21,21)
COMMON/2/OMA(21,21,21)
COMMON N,NPLUS1,M,MPLUS1,NZ,MP,NT,NTPLUS1
DIMENSION DT(21)
READ 300,N,M,NT
300  FORMAT(3I2)
      MPLUS1=M+1
      MMESH=M-1
      JM=0
      NPLUS1=N+1
      NMESH=N-1
      H=1./N
      H2=H*H
      DDT=1./2.
      NTPLUS1=NT+1
      NTMESH=NT-1
      DO 818 I=1,NTPLUS1
818  DT(I)=DDT
      EPS=.001
C    INITIALIZE VECTORS
      NZ=0
      KJ=0
      MP=5
      ISTOP=0
      R=500
      C1=.7
      F1=.3
      RW=1.0
104  CONTINUE
      KJ=0
      PRINT 2323,C1
2323 FORMAT(1H1,F8.2)
      DO 1 K=1,NTPLUS1
      DO 1 I=1,NPLUS1
      DO 1 J=1,MPLUS1
      SVOUT(I,J,K)=0
      SVPSI(I,J,K)=0
      PSI(I,J,K)=0
1    OMA(I,J,K)=0
      NM=0
      F2=1-F1
      C2=1-C1
      K=NT+1
C    READ IN STEADY STATE SOLUTION
      NE=0
      NN=7
      DO230 JP=1,NPLUS1,7
      NB=JP
      NE=NE+NN
      IF(NE .GT. NPLUS1)231,232
231  NE=NPLUS1
232  DO230 J=1,MPLUS1

```

```
L=MPLUS1-J+1
READ 233,(PSI(I,L,K),I=NB,NE)
```

```
230 CONTINUE
```

```
233 FORMAT(7F10.6)
```

```
NE=0
```

```
NN=7
```

```
DO240 JP=1,NPLUS1,7
```

```
NB=JP
```

```
NE=NE+NN
```

```
IF(NE .GT. NPLUS1)241,242
```

```
241 NE=NPLUS1
```

```
242 DO240 J=1,MPLUS1
```

```
L=MPLUS1-J+1
```

```
READ 233,(OMA(I,L,K),I=NB,NE)
```

```
240 CONTINUE
```

```
C BEGIN LOOP FOR OUTER ITERATIONS
```

```
C SAVE VORTICITY FUNCTION FROM PREVIOUS OUTER ITERATION
```

```
23 DO 40 K=2,NT
```

```
DO 40 I=1,NPLUS1
```

```
DO 40 J=1,MPLUS1
```

```
40 SVOUT(I,J,K)=OMA(I,J,K)
```

```
NM=NM+1
```

```
C BEGIN INNER ITERATION FOR STREAM FUNCTION
```

```
C COMPUTE STREAM FUNCTION FOR INNER REGION
```

```
DO 114 K=2,NT
```

```
NCOUNT=0
```

```
11 DO 2 I=3,NMESH
```

```
DO 2 J=3,MMESH
```

```
SVPSI(I,J,K)=PSI(I,J,K)
```

```
2 PSI(I,J,K)=(-.8*PSI(I,J,K))+.45*(PSI(I,J-1,K)+PSI(I,J+1,K)+PSI(I-1,J,K)+PSI(I+1,J,K)+H2*OMA(I,J,K))
```

```
C COMPUTE STREAM FUNCTION ON TOP AND BOTTOM INNER BOUNDARY LINES
```

```
DO 3 I=2,N
```

```
PSI(I,M,K)=.25*PSI(I,MMESH,K)+.5*H
```

```
3 PSI(I,2,K)=(.25*PSI(I,3,K))
```

```
C COMPUTE STREAM FUNCTION ON LEFT AND RIGHT INNER BOUNDARY LINES
```

```
DO 4 I=3,MMESH
```

```
PSI(2,I,K)=.25*PSI(3,I,K)
```

```
4 PSI(N,I,K)=.25*PSI(N-1,I,K)
```

```
C TEST STREAM FUNCTION FOR CONVERGENCE
```

```
DO 5 I=3,NMESH
```

```
DO 5 J=3,MMESH
```

```
DIFF=ABSF(SVPSI(I,J,K)-PSI(I,J,K))
```

```
IF(DIFF .GT. EPS) GO TO 6
```

```
5 CONTINUE
```

```
C RECALCULATE STREAM FUNCTION USING WEIGHTING
```

```
DO 222 I=3,NMESH
```

```
DO 222 J=3,MMESH
```

```
222 PSI(I,J,K)=F1*SVPSI(I,J,K)+F2*PSI(I,J,K)
```

```
114 CONTINUE
```

```
GO TO 200
```

```
6 NCOUNT=NCOUNT+1
```

```
IF(NCOUNT .GT. 100) GO TO 8
```

```
GO TO 11
```

```
C TEST STREAM FUNCTION FOR DIVERGENCE
```

```

8     IF(DIFF .GT. 10) GO TO 28
      PRINT 93
93    FORMAT(1H1,11H PSI VALUES)
      CALL PRNTLST(PST)
10    FORMAT(10F11.6)
      NCOUNT=0
      GO TO 11
28    PRINT 81
81    FORMAT(13H PSI DIVERGED)
      CALL PRNTLST(PST)
      CALL PRNTLST(OMA)
      GO TO 699
C     BEGIN INNER ITERATION FOR VORTICITY
200   NCOUNT=0
30    HCONST=C2*(-2./H2)
C     COMPUTE VORTICITY ON BOUNDARY LINES USING WEIGHTING
C     TOP AND BOTTOM BOUNDARY LINES
      DO 12 K=2,NT
        DO 12 I=1,NPLUS1
          OMA(I,M+1,K)=C1*OMA(I,M+1,K)+HCONST*(PST(I,M,K)-H)
12    OMA(I,1,K)=C1*OMA(I,1,J)+HCONST*PST(I,2,K)
C     LEFT AND RIGHT BOUNDARY LINES
      DO 13 K=2,NT
        DO 13 I=2,M
          OMA(1,I,K)=HCONST*PST(2,I,K)+C1*OMA(1,I,K)
13    OMA(N+1,I,K)=HCONST*PST(N,I,K)+C1*OMA(N+1,I,K)
90    CONTINUE
C     COMPUTE COEFFICIENTS FOR VORTICITY EQUATIONS
C     COMPLETE ONE SWEEP OF INTERIOR
      DO 14 K=2,NT
        DO 14 I=2,N
          DO 14 J=2,M
            A1=PST(I+1,J,K)-PST(I-1,J,K)
            B1=PST(I,J+1,K)-PST(I,J-1,K)
            A=ABSF(A1)
            B=ABSF(B1)
            W0=((4*R*H2+8*DT(K))/(2*DT(K)))+(A+B)*(R/2)
            HNEW=(R*H2)/(2*W0*DT(K))
            RNEW=1/W0
            IF(A1.GE. 0)15,16
15    W2=1+(R/2)*A
            W4=1
            GO TO 17
16    W2=1
            W4=1+A*(R/2)
17    IF(B1.GE. 0)18,19
18    W1=1
            W3=1+B*(R/2)
            GO TO 20
19    W1=1+B*(R/2)
            W3=1
20    SVPSI(I,J,K)=OMA(I,J,K)
            IF(ISTOP .EQ. 1)GO TO 305
            OMA(I,J,K)= (RNEW*(W1*OMA(I+1,J,K)+W2*OMA(I,J+1,K)+W3*OMA(I-1,
1J,K)+W4*OMA(I,J-1,K)) +HNEW*(3*OMA(I,J,K-1)+OMA(I,J,K+1)))*RW+(1-

```

2RW)\*OMA(I,J,K)

GO TO 14

C CHECK TO SEE IF DIFFERENCE EQUATIONS ARE SATISFIED TO EPS1

305 DIFF= (RNEW\*(W1\*OMA(I+1,J,K)+W2\*OMA(I,J+1,K)+W3\*OMA(I-1,  
1J,K)+W4\*OMA(I,J-1,K)) +HNEW\*(3\*OMA(I,J,K-1)+OMA(I,J,K+1)))-OMA(I,J  
2,K)

DIF=ABSF(DIFF)

IF(DIF .GT. EPS1)282,14

282 PRINT 183,I,J,K

GO TO 700

14 CONTINUE

IF (ISTOP .EQ. 1) GO TO 700

C TEST VORTICITY FOR CONVERGENCE

DO 21 K=2,NT

DO 21 I=2,N

DO 21 J=2,M

DIFF=ABSF(SVPSI(I,J,K)-OMA(I,J,K))

IF(DIFF .GE. EPS) GO TO 22

21 CONTINUE

C RECALCULATE VORTICITY USING WEIGHTING

DO 144 K=2,NT

DO 144 I=2,N

DO 144 J=2,M

144 OMA(I,J,K)=C1\*SVPSI(I,J,K)+C2\*OMA(I,J,K)

JM=JM+1

C PRINT OUT EVERY 2 OUTER ITERATES

IF(JM .EQ. 2)89,59

89 JM=0

PRINT 79,NM

79 FORMAT(1H1,I2,17H OUTER ITERATIONS)

PRINT 91

CALL PRNTLST(Psi)

PRINT 92

CALL PRNTLST(OMA)

C TEST OUTER ITERATIONS FOR CONVERGENCE

59 CONTINUE

DO 45 K=2,NT

DO 45 I=1,NPLUS1

DO 45 J=1,MPLUS1

DIFF=ABSF(SVOUT(I,J,K)-OMA(I,J,K))

IF(DIFF .GT. EPS) GO TO 7

45 CONTINUE

NZ=1

PRINT 99,NM

99 FORMAT(1H1,22H PROBLEM CONVERGED IN ,I4)

PRINT 91

91 FORMAT(1X,11H PSI VALUES)

CALL PRNTLST(Psi)

PRINT 92

92 FORMAT(1H1,14H OMEGA VALUES)

CALL PRNTLST(OMA)

EPS1=.001

RMAX=0

ISTOP=1

C CHECK TO SEE IF DIFFERENCE EQUATIONS FOR STREAM FUNCTION ARE SATISFIED TO

```

C   A TOLERANCE OF EPS1
DO 181 KK=2,NT
DO 181 II=3,NMESH
DO 181 JJ=3,MMESH
A=-4*PSI(II,JJ,KK)+PSI(II+1,JJ,KK)+PSI(II,JJ+1,KK)+PSI(II-1,JJ,KK)+
1+PSI(II,JJ-1,KK)
B=-H*H*OMA(II,JJ,KK)
D=A-B
IF(D.GT.EPS1) GO TO 182
181  CONTINUE
GO TO 90
182  PRINT 183,II,JJ,KK
183  FORMAT(1H1,41H DIFFERENCE EQU. NOT SATISFIED AT POINT (,I2,1H,,I2
1,1H,,I2,1H))
GO TO 699
C   TEST OUTER ITERATIONS FOR DIVERGENCE
7    IF(DIFF.GT.100)199,23
22   NCOUNT=NCOUNT+1
IF(NCOUNT.GT.300) GO TO 24
GO TO 90
C   TEST VORTICITY FOR DIVERGENCE
24   IF(DIFF.GT.10) GO TO 29
PRINT 94
94   FORMAT(1H1,14H OMAEGA VALUES)
CALL PRNTLST(OMA)
PRINT 91
CALL PRNTLST(PSI)
32   FORMAT(10F11.6)
NCOUNT=0
GO TO 90
29   PRINT 82
82   FORMAT(13H OMA DIVERGED)
CALL PRNTLST(PSI)
CALL PRNTLST(OMA)
GO TO 699
199  PRINT 189
189  FORMAT(26H OUTER ITERATIONS DIVERGED)
699  CONTINUE
700  CONTINUE
PRINT 303,RMAX
303  FORMAT(1H1,17H PSI CONVERGED TO,E12.4)
END

```

